

----- THESIS -----

---KENNETH C. McCARTER. ---

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--CALIFORNIA INSTITUTE OF TECHNOLOGY.--

--PASADENA, CALIFORNIA.--

----COMMERCIAL TESTING OF CONCRETE.----

The material included within this report is the result of a series of tests of concrete specimens taken during the construction of various buildings in the cities of Pasadena and Los Angeles over a period of eight months.

The object of the problem is to determine the effect of the water ratio on the ultimate strength of the concrete as obtained from data observed and recorded from specimens taken from actual building practice rather than that from laboratory specimens made under ideal ,or at least more nearly standard conditions.

The conclusions are drawn in a tabular form on page 10.

It was also observed that about eight out of every ten contractors are using admixtures to the extent of about three per cent by weight of the cement used .

The strength of specimens tested at seven days were evaluated for comparative purposes to their probable strength at twentyeight days by Abrams diagram formula:

Strength(28 days) is equal to Strength (7 days) * plus 30 times square root of Strength (7 days).

All specimens taken are for a nominal mix of $1:2\frac{1}{4} : 3\frac{1}{4}$.

| Spec No. | Cast | Tested | Days | Slump. | *sg in (7 days) | *sg in (28 days) |
|----------|------|--------|------|--------|--------------------|---------------------|
| 1. | 3/4 | 4/3 | 29 | 9 | | 1700 |
| 2. | 3/4 | 4/3 | 29 | 9 | | 1220 |
| 3 | 3/4 | 4/3 | 29 | 8 | | 1400 |
| 4 | 3/4 | 4/3 | 29 | 8 | | 1470 |
| 5 | 3/5 | 4/3 | 28 | 6 | | 1900 |
| 6 | 3/5 | 4/3 | 28 | 5 | | 1720 |
| 7 | 3/5 | 4/3 | 28 | 9 | | 1645 |
| 8 | 3/5 | 4/3 | 28 | 7 | | 1850 |
| 9 | 3/6 | 4/4 | 28 | 5 | | 1420 |
| 10 | 3/6 | 4/4 | 28 | 9 | | 1360 |
| 11 | 3/6 | 4/4 | 28 | 7 | | 1335 |
| 12 | 3/6 | 4/4 | 28 | 7 | | 1356 |
| 13 | 1/27 | 2/25 | 29 | 10 | | 1050 |
| 14 | 1/27 | 2/25 | 29 | 10 | | 1400 |
| 15 | 3/25 | 4/22 | 28 | 3 | | 2350 |
| 16 | 3/25 | 4/22 | 28 | 3 | | 2600 |
| 17 | 3/25 | 4/22 | 28 | 3 | | 2375 |
| 18 | 3/20 | 4/22 | 33 | 4 | | 2230 |
| 19 | 3/25 | 4/22 | 28 | 4 | | 2210 |
| 20 | 3/26 | 4/23 | 28 | 5 | | 1925 |
| 21 | 3/26 | 4/23 | 28 | 3 | | 2430 |
| 22 | 3/26 | 4/23 | 28 | 4 | | 2360 |

| Spec No. | Cast | Test | Days | Slump | #/sq in. (7 days) | #/sq in. (28 days) | |
|----------|------|------|------|-------|----------------------|-----------------------|---------|
| 23 | 3/26 | 4/23 | 28 | 3 | | 2695 | |
| 24 | 3/26 | 4/23 | 28 | 3 | | 2885 | |
| 25 | 3/26 | 4/23 | 28 | 4 | | 2220 | |
| 26 | 3/31 | 5/5 | 35 | 3 | | 2825 | |
| 27 | 4/16 | 5/15 | 29 | 9 | | 1130 | |
| 28 | 4/16 | 5/15 | 29 | 6 | | 1730 | |
| 29 | 4/17 | 5/15 | 28 | 9 | | 1300 | |
| 30 | 4/17 | 5/15 | 28 | 9 | | 1420 | |
| 31 | 4/17 | 5/15 | 28 | 11 | | 925 | |
| 32 | 4/17 | 5/15 | 28 | 8 | | 1660 | |
| 33 | 4/27 | 5/5 | 8 | 4 | 1595 | 2795 | |
| 34 | 4/27 | 5/5 | 8 | 4 | 1530 | 2710 | |
| 35 | 4/28 | 5/5 | 7 | 4 | 1322 | 2412 | |
| 36 | 4/29 | 5/6 | 7 | 5 | 1133 | 2138 | |
| 37 | 5/1 | 5/8 | 7 | 6 | 1535 | 2710 | 1% D.E. |
| 38 | 5/1 | 5/8 | 7 | 4 | 1358 | 2460 | 2% D.E. |
| 39 | 5/1 | 5/8 | 7 | 5 | 1353 | 2460 | 3% D.E. |
| 40 | 5/3 | 5/10 | 7 | 4 | 1560 | 2745 | |
| 41 | 5/8 | 5/15 | 7 | 5 | 1400 | 2525 | |
| 42 | 5/8 | 5/15 | 7 | 4 | 1602 | 2802 | |
| 43 | 5/8 | 5/15 | 7 | 5 | 1482 | 2632 | |
| 44 | 4/19 | 5/17 | 28 | 6 | | 2245 | |
| 45 | 4/19 | 5/17 | 28 | 4 | | 1818 | |

| Spec. No. | Cast | Test | Days | Slump. | */sq in (7 day) | */sq in (28 day) | |
|-----------|------|------|------|--------|--------------------|---------------------|---------|
| 46 | 4/19 | 5/17 | 28 | 5 | | 2020 | |
| 47 | 4/20 | 5/18 | 28 | 4 | | 3210 | |
| 48 | 4/21 | 5/19 | 28 | 3 | | 3215 | |
| 49 | 4/22 | 5/20 | 28 | 4 | | 2900 | |
| 50 | 4/22 | 5/20 | 28 | 3 | | 3285 | |
| 51 | 5/13 | 5/20 | 7 | 2 | 2075 | 3445 | |
| 52 | 4/26 | 5/24 | 28 | 4 | | 2495 | |
| 53 | 4/26 | 5/24 | 28 | 4 | | 2900 | |
| 54 | 4/27 | 5/25 | 28 | 4 | | 2535 | |
| 55 | 4/27 | 5/25 | 28 | 3 | | 3375 | |
| 56 | 4/28 | 5/26 | 28 | 4 | | 2620 | |
| 57 | 4/30 | 5/28 | 28 | 4 | | 2421 | |
| 58 | 5/21 | 5/28 | 7 | 6 | 1500 | 2660 | |
| 59 | 5/21 | 5/28 | 7 | 6 | 1568 | 2758 | |
| 60 | 5/21 | 5/28 | 7 | 6 | 1661 | 2880 | |
| 61 | 5/1 | 5/29 | 28 | 4 | | 2140 | 1% D.E. |
| 62 | 5/1 | 5/29 | 28 | 3 | | 3160 | 2% D.E. |
| 63 | 5/1 | 5/29 | 28 | 5 | | 2080 | 3% D.E. |
| 64 | 5/24 | 5/31 | 7 | 3 | 1728 | 2980 | |
| 65 | 5/24 | 5/31 | 7 | 4 | 1588 | 2790 | |
| 66 | 5/24 | 5/31 | 7 | 4 | 1660 | 2880 | |
| 67 | 5/28 | 6/4 | 7 | 4 | 1623 | 2830 | |
| 68 | 5/28 | 6/4 | 7 | 6 | 1438 | 2580 | |

| Spec. No. | Cast | Test | Days | Slump. | */sq in (7 day) | */sq in (28 day) |
|-----------|------|------|------|--------|--------------------|---------------------|
| 69 | 5/28 | 6/4 | 7 | 4 | 1567 | 2760 |
| 70 | 4/21 | 4/28 | 7 | 3 | 1640 | 2850 |
| 71 | 4/21 | 4/28 | 7 | 3 | 1560 | 2750 |
| 72 | 4/1 | 4/29 | 28 | 3 | | 3000 |
| 73 | 4/1 | 4/29 | 28 | 3 | | 2975 |
| 74 | 4/1 | 4/29 | 28 | 3 | | 2890 |
| 75 | 4/1 | 4/29 | 28 | 3 | | 3065 |
| 76 | 4/20 | 5/4 | 14 | 3 | 2278 | 2993 |
| 77 | 4/20 | 5/4 | 14 | 5 | 1942 | 2600 |
| 78 | 4/20 | 5/4 | 14 | 6 | 1525 | 2110 |
| 79 | 4/20 | 5/4 | 14 | 3 | 2272 | 2987 |
| 80 | 5/7 | 5/15 | 8 | 6 | 1400 | 2520 |
| 81 | 5/7 | 5/15 | 8 | 7 | 1075 | 2055 |
| 82 | 5/7 | 5/15 | 8 | 6 | 1108 | 2100 |
| 83 | 5/7 | 5/15 | 8 | 7 | 1025 | 1985 |
| 84 | 4/20 | 5/18 | 28 | 3 | | 2522 |
| 85 | 4/20 | 5/18 | 28 | 3 | | 2660 |
| 86 | 4/20 | 5/18 | 28 | 3 | | 2530 |
| 87 | 4/20 | 5/18 | 28 | 3 | | 2520 |
| 88 | 4/20 | 5/18 | 28 | 4 | | 2400 |
| 89 | 4/20 | 5/18 | 28 | 6 | | 1782 |
| 90 | 5/6 | 6/4 | 28 | 5 | | 2050 |
| 91 | 5/6 | 6/4 | 28 | 4 | | 2410 |

| Spec No. | Cast | Test | Days | Slump | */sg in. (7 day) | */sg in. (28 day) | |
|----------|-------|------|------|-------|---------------------|----------------------|--------|
| 92 | 5/6 | 4/4 | 28 | 3 | | 2810 | |
| 93 | 5/6 | 6/4 | 28 | 6 | | 2250 | |
| 94 | 11/11 | 12/9 | 28 | 7 | | 1720 | |
| 95 | 11/13 | 2/16 | 90 | 8 | | 1250 | |
| 96 | 11/13 | 2/16 | 90 | 12 | | 980 | 3% DE. |
| 97 | 11/13 | 2/16 | 90 | 6 | | 1485 | 3% DE. |
| 98 | 11/13 | 2/16 | 90 | 8 | | 1700 | |

Slump 2 3 4 5 6 7 8 9 10 11 12

| Spec. No. | | | | | | | | | | | |
|-----------|-------|-------|-------|-------|-------|-------|------|------|------|-----|-----|
| 1 | | | | | | | | 1700 | | | |
| 2 | | | | | | | | 1220 | | | |
| 3 | | | | | | | 1400 | | | | |
| 4 | | | | | | | 1470 | | | | |
| 5 | | | | | 1900 | | | | | | |
| 6 | | | | 1720 | | | | | | | |
| 7 | | | | | | | | 1645 | | | |
| 8 | | | | | | 1850 | | | | | |
| 9 | | | | 1420 | | | | | | | |
| 10 | | | | | | | | 1360 | | | |
| 11 | | | | | | 1335 | | | | | |
| 12 | | | | | | 1356 | | | | | |
| 13 | | | | | | | | | 1050 | | |
| 14 | | | | | | | | | 1400 | | |
| 15 | | 2350 | | | | | | | | | |
| 16 | | 2600 | | | | | | | | | |
| 17 | | 2375 | | | | | | | | | |
| 18 | | | 2230 | | | | | | | | |
| 19 | | | 2210 | | | | | | | | |
| 20 | | | | 1925 | | | | | | | |
| 21 | | 2430 | | | | | | | | | |
| 22 | | | 2360 | | | | | | | | |
| 23 | | 2695 | | | | | | | | | |
| 24 | | 2885 | | | | | | | | | |
| 25 | | | 2220 | | | | | | | | |
| 26 | | 2825 | | | | | | | | | |
| 27 | | | | | | | | 1130 | | | |
| 28 | | | | | 1720 | | | | | | |
| 29 | | | | | | | | 1300 | | | |
| 30 | | | | | | | | 1400 | | | |
| 31 | | | | | | | | | | 925 | |
| 32 | | | | | | | 1660 | | | | |
| 33 | | | 2795 | | | | | | | | |
| 34 | | | 2710 | | | | | | | | |
| 35 | | | 2412 | | | | | | | | |
| 36 | | | | 2138 | | | | | | | |
| 37 | | | | | 2710 | | | | | | |
| 38 | | | 2460 | | | | | | | | |
| 39 | | | | 2460 | | | | | | | |
| 40 | | | 2745 | | | | | | | | |
| 41 | | | | 2525 | | | | | | | |
| 42 | | | 2802 | | | | | | | | |
| 43 | | | | 2632 | | | | | | | |
| 44 | | | | | 2245 | | | | | | |
| 45 | | | 1818 | | | | | | | | |
| 46 | | | | 2020 | | | | | | | |
| 47 | | | 3210 | | | | | | | | |
| 48 | | 3215 | | | | | | | | | |
| 49 | | | 2900 | | | | | | | | |
| | 34415 | 40727 | 32872 | 23570 | 21710 | 10201 | 7480 | 9755 | 2400 | 925 | 780 |

Slump 2 3 4 5 6 7 8 9 10 11 12

| Spec No. | | | | | | | | | | | |
|----------|------|------|------|------|-------|------|------|------|--|--|-----|
| 50 | | 3285 | | | | | | | | | |
| 51 | 3445 | | | | | | | | | | |
| 52 | | | 2495 | | | | | | | | |
| 53 | | | 2900 | | | | | | | | |
| 54 | | | 2535 | | | | | | | | |
| 55 | | 3375 | | | | | | | | | |
| 56 | | | 2620 | | | | | | | | |
| 57 | | | 2421 | | | | | | | | |
| 58 | | | | | | 2660 | | | | | |
| 59 | | | | | | 2758 | | | | | |
| 60 | | | | | | 2880 | | | | | |
| 61 | | | 2140 | | | | | | | | |
| 62 | | 3160 | | | | | | | | | |
| 63 | | | | 2080 | | | | | | | |
| 64 | | 2980 | | | | | | | | | |
| 65 | | | 2790 | | | | | | | | |
| 66 | | | 2880 | | | | | | | | |
| 67 | | | 2830 | | | | | | | | |
| 68 | | | | | | 2580 | | | | | |
| 69 | | | 2760 | | | | | | | | |
| 70 | | 2850 | | | | | | | | | |
| 71 | | 2750 | | | | | | | | | |
| 72 | | 3000 | | | | | | | | | |
| 73 | | 2975 | | | | | | | | | |
| 74 | | 2890 | | | | | | | | | |
| 75 | | 3065 | | | | | | | | | |
| 76 | | 2993 | | | | | | | | | |
| 77 | | | | 2600 | | | | | | | |
| 78 | | | | | | 2110 | | | | | |
| 79 | | 2987 | | | | | | | | | |
| 80 | | | | | | 2520 | | | | | |
| 81 | | | | | | | 2055 | | | | |
| 82 | | | | | | 2100 | | | | | |
| 83 | | | | | | | 1985 | | | | |
| 84 | | 2522 | | | | | | | | | |
| 85 | | 2660 | | | | | | | | | |
| 86 | | 2530 | | | | | | | | | |
| 87 | | 2520 | | | | | | | | | |
| 88 | | | 2400 | | | | | | | | |
| 89 | | | | | | 1782 | | | | | |
| 90 | | | | 2050 | | | | | | | |
| 91 | | | 2410 | | | | | | | | |
| 92 | | 2810 | | | | | | | | | |
| 93 | | | | | | 2250 | | | | | |
| 94 | | | | | | | 1720 | | | | |
| 95 | | | | | | | | 1250 | | | |
| 96 | | | | | | | | | | | 980 |
| 97 | | | | | | 1485 | | | | | |
| 98 | | | | | | | | 1700 | | | |
| | 5465 | 4935 | 6415 | 6730 | 23125 | 2760 | 2150 | | | | |

| Slump (inches) | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|-------------------|------|-------|-------|-------|-------|-------|------|------|------|-----|-----|
| Summation | 3445 | 70725 | 64054 | 23570 | 31700 | 10301 | 7480 | 9755 | 2450 | 925 | 980 |
| Number Specimens | 1 | 25 | 25 | 11 | 14 | 6 | 5 | 7 | 2 | 1 | 1 |
| Average */sq.in. | 3445 | 2830 | 2565 | 2150 | 2260 | 1720 | 1500 | 1400 | 1225 | 925 | 980 |
| Maximum | — | 3375 | 3210 | 2632 | 2880 | 2055 | 1700 | 1700 | 1400 | — | — |
| % > average | — | 19 | 25 | 22 | 27 | 20 | 13 | 21 | 14 | — | — |
| Minimum | — | 2350 | 1818 | 1420 | 1485 | 1335 | 1250 | 1130 | 1050 | — | — |
| % < average | — | 17 | 29 | 34 | 34 | 22 | 17 | 19 | 14 | — | — |